# Hardenability and corroson resistance of as cast Fe-9AI-0,6C alloy

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#### ABSTRACT

On the basis of economic considerations, Fe-Al-C alloy could be a good candidate for replacing some of the conventional stainless steel. Wherein, Al is used to replace the expensive alloy element in conventional Fe-Cr-C system. The aim of the research is to investigate harden ability and corrosion resistance of Fe-9Al-0,6C in the NaCl and  $H_2SO_4$  solution. Thirty five kilograms of Fe-Al-C were prepared from mild steel scrap, high purity aluminium, and Fe-C. The alloy was prepared in an induction furnace under an argon atmosphere. Jominy test and microstructure were examined. And, the corrosion rate, were carried out with three-electrode polarization in 0.5% NaCl and 0.05M  $H_2SO_4$ . The corrosion type and the morphology of the oxide scale were examined with EDS/EDAX. The optical micrograph shows that as cast Fe-9Al-0,6C alloy has ferrite and pearlite microstructure. The result of Jominy test shows that these alloy non-harden able. The result of corrosion testing showed that the alloy more resistance in NaCl than in  $H_2SO_4$  solution. Optical micrograph and SEM analysis indicated that corrosion form is general corrosion and there is no trend toward intergranular attack.

Key words: Fe-Al-C alloy, conventional stainless steel, harden ability, corrosion resistance.

### INTRODUCTION

Fe-AI-C alloy is being developed for elevated temperature structural application up to 873K<sup>2-4</sup>. In addition, the plain iron-aluminum lightweight steel containing up to 9 wt-% Al shows a reduction in density of 10% and more<sup>1</sup>. On the basis of economic and lower density considerations, this material could be a good candidate for replacing some of the conventional stainless steel<sup>5-6</sup>. Wherein, Al is used to replace the expensive alloy element (Cr) in conventional Fe-Cr-C system.

Ferritic iron aluminum is show promising physical, mechanical and technological properties, corrosion and oxidation resistance, and low raw material cost<sup>2</sup> which is suitable for development and design of new type of high strength lightweight steel<sup>3</sup>. In addition, the plain iron-aluminum lightweight steel containing up to 9 wt-% Al shows a reduction in density of 10% and more.

In contrast, Fe-Al alloys exhibit poor toughness and brittle behavior at room temperature. Recent studies indicate that reduction in Al content to 8.5 wt-% resulted in enhanced ductility. In previous work, it has been shown that low carbon content (0.05 and 0.1 wt-%) in Fe-9 wt-% Al leads low tensile ductility7. Addition of carbon to Fe-Al containing 8.5 to 16 wt-%Al leds to higher strength<sup>5</sup>, and better machinability<sup>[6]</sup>. It has been shown that low carbon content (0.05 and 0.1 wt-%) in Fe-9 wt-% Al leads low tensile ductility7. Whereas, the ESR ingots of Fe-10.5Al and Fe-13Al alloys containing high (0.5 and 1.0 wt-%) carbon exhibit excellent hot workability8. The Fe-10.5 wt-%Al and Fe-13 wt-%Al alloys with low carbon content (0.05 and 0.1 wt-%) exhibit the presence of fine needle shaped Fe3AIC0.5 precipitates in the matrix and along the grain boundaries8.

Fe-Al-C alloy is being developed for elevated temperature structural application up to 873K<sup>9,10</sup>.

Aluminum plays a major role in the oxidation and corrosion resistance which is characteristic of the binary Fe-Al alloy<sup>11</sup>. The Fe-Al-C alloys have good corrosion resistance in a neutral environments and were corrode at rates comparable to that of white cast-iron in acid environments<sup>12</sup>. However, few data are available on the corrosion phenomena of Fe-Al alloy in acid media like H<sub>2</sub>SO<sub>4</sub>.

In this study, harden ability and corrosion behavior of Fe-9AI-0.6C alloy have been reported.

#### MATERIAL AND METHODS

Thirty five kilograms of Fe-AI-C were prepared from mild steel scrap, high purity aluminum, and Fe-C. The alloy was prepared in a high frequency induction furnace under a controlled protective argon atmosphere. The chemical compositions are listed in Table 1. The ingot was cut using bimetallic band saw blade to make the Jominy specimen (EN ISO 642 standard) and the corrosion specimen (14 mm in gauge diameter and 3 mm in gauge length). Microstructures of as cast alloys were examined by using an optical and electron microscope. The possible phases present in the diffraction specimens were identified using X-ray diffraction with a copper target, nickel filter and a graphite single crystal monochromater.

The surface of the corrosion specimens were mechanically polished with abrasive paper up to 1200 grit, after surface finishing. The last mechanical polishing was done with 0.5 5 $\mu$ m alumina paste. The corrosion rate were carried out with three-electrode polarization in 0.5% NaCl and 0.05M H<sub>2</sub>SO<sub>4</sub>. The corrosion type and the morphology of the oxide scale were examined by optical microscopy and scanning electron microscope (SEM). Corrosions product were examined with EDS/EDAX.

The polished section were subsequently etched with 3.3% HNO3-3.3% CH3COOH-0.1% Hf-93.3% H2O by volume for micro structural examination by optical microscope.

#### **RESULTS AND DISCUSSION**

#### Harden ability analysis

Table 2 shows the hardness value after Jominy test. Figure 1 shows hardness distribution of Fe-9AI-0.6C alloys curve after Jominy test. There

Alloys	AI	С	Mn	Si	Р	S	Fe
В	9.00	0.6	0.66	0.18	0.03	0.02	Bal.

Table 1: Chemical composition (wt-%) of the alloy tested

Table 2: Hardness value (VHN) of as cast Fe-9AI-0,6C alloy after Jominy test

Distance from the top of Jominy test spesimen (mm)	Hardness (VHN)
0,2	300
1	299.9
2	299.9
5	299.5
10	298.5
20	298.5
30	299.5
50	296.2
80	296.2

is no significantly increasing hardness. Figure 2 shows the microstructure of as cast Fe-9Al-0.6C alloy. The as cast Fe-9Al-0.6C alloy is composed of  $\alpha$ -Fe and pearlites. It has been known that Al was stabilized ferrite phase <sup>[10]</sup> but appearance of pearlites structure because of the content of C.

Figure 3 shows the microstructure of as cast Fe-9AI-0.6C alloys after Jominy test. The as cast Fe-9AI-0.6C alloy microstructures are full ferritic. Pearlite structure is decomposed to ferrite structure after heating and then rapid cooling on the Jominy test. Because of cooling rate differentiation, microstructure of as cast Fe-9AI-0.6C alloy differents from the top toward to the end of

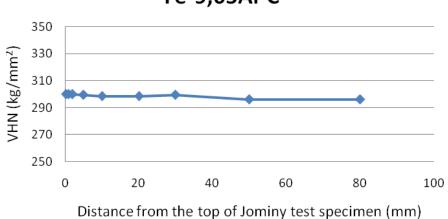




Fig. 1: Hardness distribution of as cast Fe-9AI-0,6C alloy after Jominy test

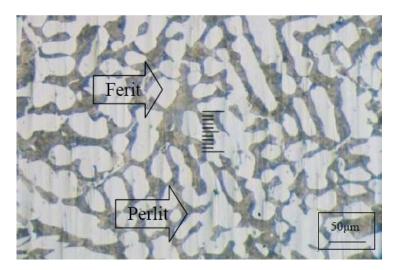
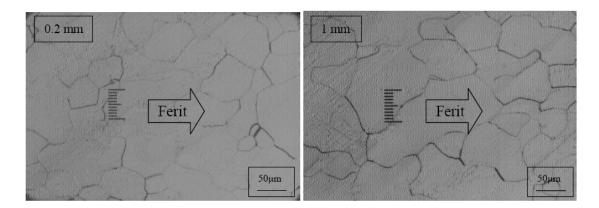


Fig. 2: Microstructure of as cast Fe-9AI-0,6C alloy



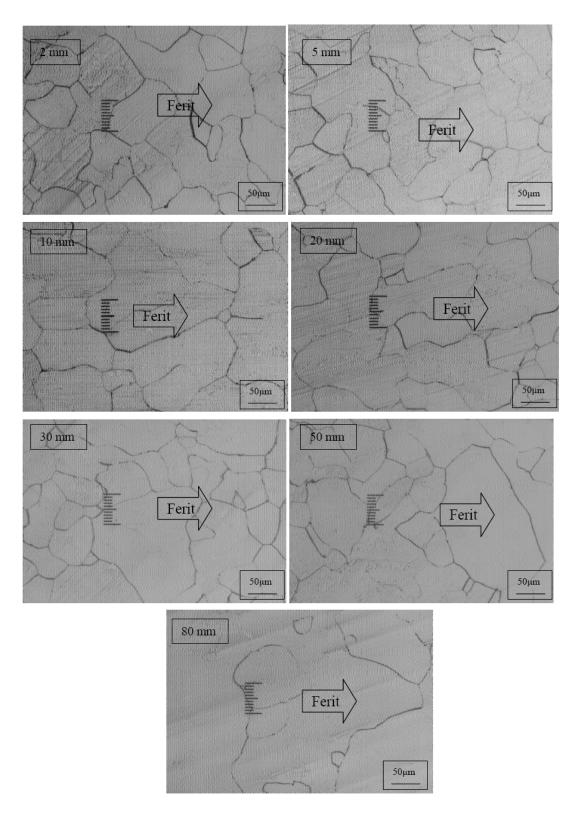


Fig. 3: Microstructure of the as cast Fe-9AI-0,6C alloy after Jominy test

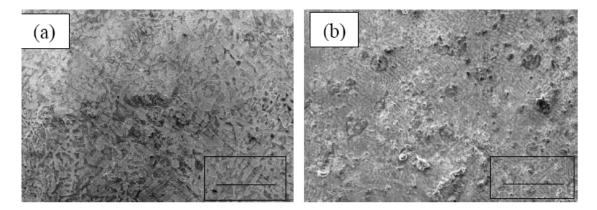


Fig. 4: SEM micrographs of the as cast Fe-9Al-0.6C alloy after corroded (a). in 0.05 M  $H_2SO_4$  b. in 0.5% NaCl solution

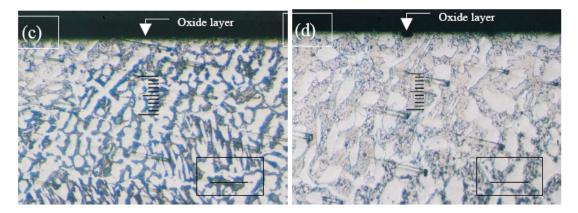


Fig. 5: Metallographics cross section of the as cast Fe-9AI-0.6C alloy after corroded (a). in 0.05 M  $H_2SO_4$  (b). in 0.5% NaCI solution

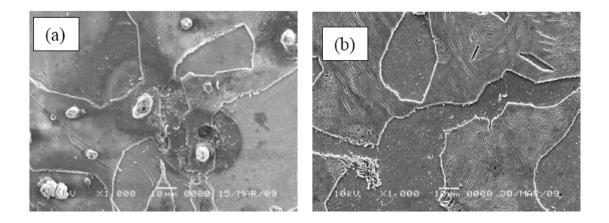


Fig. 6: SEM micrographs high magnification of as the cast Fe-9AI-0.6C alloy after corroded (a). in 0.05 M  $H_2SO_4$  (b). in NaCl solution

Jominy test specimen only on the magnitude of grain. High AI content of as cast Fe-9AI-0.6C alloy caused ferrite structure stabilized. Heating of specimen was continued with quenching no change ferrite structure to martensite because of high AI content. AI was known as ferrite stabilizer, although this alloy has high C (0.6 wt%) that is not influence ferrite stabilizer. So, that is conformity between hardness distribution and microstructure after Jominy test. It can concluded that as cast Fe-9AI-0.6C alloy is non harden able with heat treatment.

#### **Corrosion Resistance analisys**

The three-electrode polarization was used to examine corrosion rate of the alloy. The result of the examination was showed in table 2. Table 2 indicates that in the 0.5% NaCl solution the corrosion rate of the as cast Fe-9AI-0.6C alloy is lower than in the 0.05 M  $H_2SO_4$  solution . The differentiation of the corrosion rate is caused solution reactivity. This corrosion rate is fair category in the 0.5% NaCl solution and poor category in the 0.05 M  $H_2SO_4$  solution<sup>14</sup>.

Figur 4. shows surface corroded for the alloys. Light and dark pattern microstructures seem at this picture. Whereas, in the higher magnification (Figur 6) oxide pattern was very clear. SEM-EDS analysis (Figur 7) shows present some oxides like  $Al_2O_3$  and FeO that are come from composition of these alloy, while  $Na_2O$ ,  $SO_3$  and CI are from corrosion medium. The micrograph cross section of as cast Fe-9Al-0.6C alloy after corroded show that the oxide layers formed on the surface of the alloy after corrosion testing (Fig 5). It was observed that thin oxide layer formed on the surface but

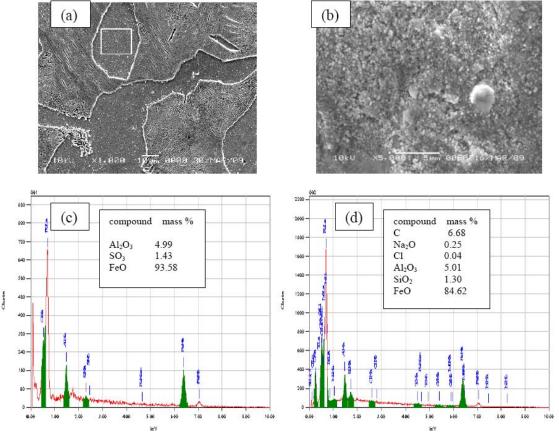


Fig. 7: SEM micrographs of the as cast Fe-9AI-0.6C alloy after corroded (a). SE image in 0.05M  $H_2SO_4$  0.05M (b). SE image in 0.5% NaCl c. EDS result in 0.05M  $H_2SO_4$  0.05M d. EDS result in 0.5% NaCl solution

Specimen	l corr (/	I corr (A/cm²)		R (mpy)		
	0.5% NaCl	0.5% H <sub>2</sub> SO <sub>4</sub>	0.5% NaCl	0.05 M H <sup>2</sup> SO <sub>4</sub>		
Fe-9Al	89.61	216.21	30.47	73.51		

Table 2: Corrosion rate of the as cast Fe-9Al-0.6C alloy

internal oxidation product could not be observed. The thickness of oxide layer of as cast Fe-9AI-0.6C alloy could be observed in both of corrosion medium. These phenomena connected with corrosion rate. General corrosion could be observed on the surface of corrosion specimen but no intergranular attack could be observed in these conditions.

## CONCLUSIONS

The as cast Fe-9AI-0.6C alloy has ferrites and pearlites microstructure. After Jominy test, microstructure this alloy change into full ferritic. The as cast Fe-9AI-0.6C alloy is non harden able with heat treatment. General corrosion could be observed after three-electrode polarization but there is no trend toward to intergranular corrosion attack.

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