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# **Study of Structural and Magnetic Properties of CuFe2 O4 Tuning by Heat Treatment**

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# **ABSTRACT**

This study evaluates the relationship with microstructural and electromagnetic properties dependences on sintering temperature of bulk Copper ferrites synthesized by the solid state reaction method calcined at  $\mathsf{T}_\mathrm{s}$  950°C, 1050°C, 1100°C and 1150°C. These properties are examined by XRD, DTA and TGA, SEM, B–H Loops Tracer, VSM and Electrometer. The affirmation of single-phase cubic spinel structured has been observed by XRD pattern for all T $_{\!\scriptscriptstyle\rm g}$ . Under the influence of heat treatment, the grain sizes escalate from 3.63 μm to 6.48 μm due to the movement of grain boundaries. Softer ferromagnetic nature of sample for all  $\mathsf{T}_\mathrm{s}$  has been signed by narrow hysteresis loops. The assessment of magnetic properties manifests that the saturation magnetization as well as permeability amplifies with  $\mathsf{T}_\mathsf{s}$  which is correlated to the increase of the grain size. Frequency dependence dielectric constant (ε′) shows the usual dielectric nature of ferromagnetic materials. The results of all these measurements clearly emphasize the effect of sintering temperature to bring a significant change in above mention properties which is a prerequisite to the materials applications.

# **Article History**

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# **Keywords**

Copper-Ferrites; Hysteresis Loop; Magnetization; Permeability; Sintering Temperature.

## **Introduction**

In the fast few decades, the magnetic materials highlight enormous curiosity to the researcher community due to the wide range of possible geometry, reasonable manufacture cost, exceptional significant feature and high sustainability for both conventional and innovative applications.1 Among various sorts of ferrites, Cu–ferrite exhibits phase

transition, semiconducting properties, electrical switching, and interesting magnetic and electrical properties with chemical and thermal stabilities.<sup>2</sup> Cu-ferrite is inverse spinel structure with following formula:

$$
\big(Cu^{2+}_xFe^{3+}_{1-x}\big)_A\big[Cu^{2+}_{1-x}Fe^{3+}_{1+x}\big]_B
$$

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where x is inversion parameter,  $x = 0$  indicates inverse spinel and  $x = 1$  indicates normal spinel. The synthesis method, heat treatment and cations distribution are the major key of tuning the degree of inversion (x). Its structure transform from tetragonal to cubic when temperature above 360°C due to Jahn–Teller distortion.3 Due to this duality phase variation under heat treatment, CuFe<sub>2</sub>O<sub>4</sub> has a great significance in wide range of applications in gas sensing, color imaging, magneto-optic recording device, magnetic refrigeration and catalytic applications.4-6 For the best performance in implementations, the most priority technological properties are saturation magnetization, coercive force, initial permeability, high dielectric constant etc. All these properties cannot get all together for any specific applications. By swing the compositions or incorporating additives or by altering preparation process or changing temperature and time, suitable composition can get for any particular applications. Among these variations, synthesis process and sintering temperature is very important to tune different properties for desired applications. Various methods for synthesizing spinel CuFe ${_{2} {\rm O}_4}$  has been reported as solid state reaction,<sup>7</sup> sol–gel,<sup>8</sup> chemical  $co-precipitation<sup>9</sup> auto-combustion symmetry$ and microwave–hydrothermal method.<sup>11</sup> Among the above mentioned methods, we have adopted solid state reaction method for synthesizing of  $\mathsf{CuFe}_{\mathbb{2}}\mathsf{O}_{\mathbb{4}}$  bulk ferrites as it is a high temperature technique which produces large scale products with cubic spinel formation of ferrite sample. There is an extensive and upgrade work list of interesting publications regarding structural, magnetic and electric properties of spinel CuFe $_2\rm O 4$  ferrites. $^{12\text{-}15}$ According to the previous literature, there are few reports not mentioned in details study of change of above mention properties due to varying different sintering temperature. The consequence of sintering temperature toward microstructural, magnetic, electric, and dielectric properties of copper ferrite is the focal points of this research work.

#### **Experimental**

Powder with a composition CuFe<sub>2</sub>O<sub>4</sub> has been synthesized through the solid state reaction method using CuO and Fe ${_{2} \mathsf{O}_{_{3}}}$  as precursors. According to the required proportion of powder were mixed and ball-milled with distilled water and zirconia balls. After dying the mixed slurry pressed into a disc shaped

and pre-sintered at 850°C for 4 hours. After crushing the pre-sintered material, powder was milled for another 4 hours in distilled water to combat in crystallites of uniform size. After drying the mixture, a few drops of saturated solution of polyvinyl alcohol were used to bind for desired shape. The powder sample molded into toroidal and pellets shapes by pressing in a stainless steel dies under a pressure of (20 KN/cm<sup>2</sup> ). The shaped specimens were dragged in the temperature range from  $950^{\circ}$ C,  $1050^{\circ}$ C, 1100 $\rm ^{\circ}C$  and 1150 $\rm ^{\circ}C$  for 2 hours. Finally, the resulting products were subjected for characterization.

The weight and dimension of the pallets were measured to determine the physical density. Phillips (PW3040) X′ Pert PRO X-ray diffractometer were used to determine phase structure of sample. Ferrite formation and microstructures has been examined by DTA & TGA using a NETZSCH DSC 201FT thermal analyzer and SEM (FEI Inspect S50) respectively. Magnetic behavior through B-H loop and M-H curve has been measured by hysteresis B-H loop tracers and VSM (EV7). Hewlett Packart Impedance Analyzer (HP 42291A) has been used to carry out the complex permeability and dielectric properties.

### **Results and discussion Structural Properties**

Phase analysis of the prepared sample has been confirmed by XRD for 950°C and 1050°C and illustrate in Figure 1 (a, b). Very intense diffraction peaks has been remarked for all sintering temperatures, indicating a good crystallinity. All the peaks of the sintered samples can be clearly indexed to the seven major peaks of the spinel ferrites, which are (2 2 0), (3 1 1), (2 2 2) (4 0 0), (4 2 2), (5 1 1) and (4 4 0) planes of a cubic unit cell. All the peaks correspond to spinel structure with no extra lines corresponding to any other phases. XRD patterns remain bearably the same at other sintering temperatures. Nien-Hsun<sup>16</sup> discovered the transformation on crystallographic CuFe ${_{2}O_{_{4}}}$  spinel structures: tetragonal phase (t-CuFe ${_{2} {\rm O}}_{4}$ ) exhibit at the low-temperature (800-900°C) where cubic phase (c- CuFe $_{2}$ O $_{4}$ ) at the high-temperature (~1000°C). Our sample also complies with their results that XRD patters shows cubic spinel structure for all sintering temperature.



Fig.1: XRD pattern of CuFe<sub>2</sub>O<sub>4</sub> sintered at (a) 950 °C and (b) 1050 °C

By using the relation:  $a = d (h^2 + k^2 + l^2) +$ , where the Miller indices of the crystal planes are h, k, and l. the lattice parameter of the samples has been enumerated. Nelson–Rilay extrapolation method has been used to determine the accurate lattice constant. The lattice constant of CuFe ${_{2} {\rm O}_4}$  is found to be 8.365 Å which is coincided with the proclaimed value 8.370 Å by Ajmal.<sup>17</sup> The physical/bulk density ( $\rho_{_{\rm B}}$ ) shrinkages from 5.12 g/cm $^3$  to 4.83 g/cm $^3$  as the temperatures are raised from 950°C to 1150°C. This decrease in bulk density may be due to the formation of pores within the grains or grain boundaries and also may be due to release of oxygen from sample during sintering.

#### **Thermal Properties**

Thermo-analytical investigations were carried out to confirm the phase formation behavior and as depicted in Figure 2. The TGA–DTA for the sample is carried out in an air atmosphere starting from  $30^{\circ}$ C on going up to a maximum temperature of 1000 $\mathrm{°C}$ . The monotonous drop in  $1<sup>st</sup>$  weight of the sample with a highest slop at around 180–185°C is observed in TGA curve which is ascribed for the evaporation of absorbed water from complex. The 2<sup>nd</sup> weight loss at 600–650° is due to release of polyvinyl +alcohol which is used as a binder. No further weight loss above 850°C was observed indicating formation of ferrite sample. Similarly, an endothermic peak observed at 70-80°C in DTA attributes to lose of absorbed water followed by a broad hump exothermic peak at around 450–550 °C imply due to removal of polyvinyl alcohol as observed in TGA

curve. Similar behavior of DTA and TGA analysis pointed by Agouriane<sup>18</sup> and Ponhan<sup>19</sup> in Cu–ferrite.



**Fig 2.DTA and TGA curve at room temperature**

#### **Microstructural Properties**

The microstructure of ferrites acts as a pivot point of monitoring of magnetic and electrical properties. Among the all microstructural parameters only grain size is more prominent for outturning the magnetic properties of ferrites. Figure 3(a–d) displays the SEM micrographs of CuFe ${_{2}O_{_{4}}}$  sintered at 950°C, 1050°C, 1100°C and 1150°C. Stoichiometric ferrites encounter regular growth of single-phase ferrite grains when sintered at higher temperature. The linear intercepts approach has been used to evaluate the average grain size and tabulated in Table 1. The increment in grain size is visible about 3.50 to

6.50 µm with upgrading temperature from 950°C to 1150°C. It is also identified that the sample sintered at 950°C appears a uniform microstructure with small grain indicating that the sintering temperature is very low for complete formation of dense microstructure. It is well-known that the formation of liquid phase is responsible for the enlargement of grain size which is also due to increase of the sintering temperatures.<sup>20</sup> During sintering, CuO forms liquid phase which influences the microstructure of the Cu-ferrites. As

a result of segregation of liquid phase to the grain boundaries, it facilitates the grain growth due to the cation interdiffusion.<sup>21</sup> During sintering, thermal energy generated a driving force which pushes the grain boundaries to grow over pores. Therefore the material becomes dense due to reduction of pore volume which leads to increase in grain size.<sup>22</sup> The values of grain size 5.3, 7.7 and 9.1 μm for sintering temperatures of 1200 °C, 1300 °C and 1400 °C has been also evaluated by Shahida<sup>23</sup> in bulk Mg-ferrite



 $(a)$  $(b)$  $(c)$  $(d)$ Fig. 3: SEM images of CuFe<sub>2</sub>O<sub>4</sub> at (a) 950 °C, (b) 1050 °C, (c) 1100 °C and (d) 1150 °C

**Table-1: Values of different measured parameters**

<b>Sintering</b> Temperature, $T_c$ (°C)	<b>Bulk</b> density, d (q/cm <sup>3</sup> )	<b>Grain</b> size, $D$ (µm)	Coercivity. $H_c$ (A/m)	B/B ratio	μ	M. $(\text{emu/g})$	<b>Resistivity,</b> ρ (ohm-cm)	ε'
$950^\circ$	5.12	3.63	517.9	0.303	34.18	35.18	$2.0 \times 10^{3}$	$6.1 \times 10^{7}$
$1050^\circ$	5.04	4.35	440.7	0.344	48.29	50.96	$2.5 \times 10^{3}$	$5.0 \times 10^{7}$
$1100^\circ$	4.95	5.42	296.3	0.442	74.52	58.09	$3.7 \times 10^{3}$	$3.7 \times 10^{7}$
$1150^\circ$	4.83	6.48	243	0.654	80.45	63.38	$5.2 \times 10^{3}$	$2.7 \times 10^{7}$

 $0.20$  $-T_s=950^{\circ}C$  $0.15$  $T = 1050^{\circ}C$  $T_s = 1100^{\circ}C$  $0.10$  $T = 1150^{\circ}C$  $\begin{array}{l} \widehat{\mathbf{a}} \\ \widehat{\mathbf{b}} \\ \widehat{\mathbf{c}} \end{array} \begin{array}{l} \textbf{0.05} \\ \textbf{0.00} \end{array}$  $\sum_{-0.05}$  $-0.10$  $-0.15$  $-0.20$  $-2000 -1500 -1000$  $-500$ 500 1000 1500 2000  $H(\AA/m)$ 

**Fig. 4: B-H** hysteresis loops of CuFe<sub>2</sub>O<sub>4</sub> at **different sintering temperature**

#### **Magnetic Properties**

Low field B-H hysteresis loops of CuFe ${_{2}O_{_{4}}}$  sintered at various temperatures is presented in Figure 4. The structural parameters as well as grain size are responsive to modify the hysteresis properties of polycrystalline ferrite. The hysteresis shape shows slanted with squat saturation induction,  $B_{s}$  which designates weak ferromagnetic phase at 950°C and 1050°C. The existing of strong ferromagnetic phase noticed due to tapered and well-defined sigmoid shape of hysteresis at 1100°C and 1150°C. With increasing calcining temperatures, the values of  $\mathsf{B}_\mathrm{s}$  increased which also demonstrates the existence of ferromagnetic phase. The values of coercivity (H<sub>c</sub>) and remanence ratio (B<sub>/</sub>/B<sub>v</sub>) has been evaluated from loops and given in Table 1. From the Figure 4, it is noticed that the narrow hysteresis loop with quite low coercivity about 520–244 A/m (6–3 Oe) indicates the soft ferromagnetic nature of ferrites system. The reduction of value of Hc has been traced mainly to enlarge in grain size with sintering temperature from 950°C – 1150°C. This change in the coercivity with sintering temperatures indicates

the relevant results by Yadav $24$  and Padampalle<sup>25</sup> in CuFe ${_{2}O_{_{4}}}$ . The remanence ratio increase from 0.34 to 0.65 with increasing sintering temperature which is consistent with the result obtained by Ponhan $^{\rm 19}$  in CuFe $_{\rm 2}$ O $_{\rm 4}$ . A low value remanence ratio (B<sub>/</sub>B<sub>v</sub>  $\approx$  0.65) is an indication of anisotropy nature of the bulk Cu-ferrite.



**Fig. 5: Frequency dependence of (a) initial and (b) imaginary permeability**

Figure 5 (a) and (b) exhibits the influence of sintering temperature (*Ts* ) on the real (*μ'*) and imaginary (μ<sup>"</sup>) permeability for CuFe<sub>2</sub>O<sub>4</sub>. As observed in Figure 5 (a), permeability expands from 34.18 to 80.45 with T $_{\rm s}$ = 950°C to 1150°C which can be ascribed to the growing in grain size leading to domain wall formation due to sintering.26 It is also noticed that the permeability is stable upto frequency 15 MHz for 950 $\degree$ C and 1050  $\degree$ C which also upto 8 MHz for 1100°C and 1150°C. At higher frequency >8 MHz, there is a small rise in permeability and falls slightly in case of last two sintering temperatures. However, the increase of  $\mathcal{T}_\mathrm{s}$  occur a decrease of magnetic anisotropy by reducing internal stress and crystal anisotropy. These reduce the impediment of movement of domain walls which results the increase of *μ'*. 27, 28 From Figure 5 (b), it is observed that imaginary permeability  $(\mu'')$  or loss tangent is almost stable for 950°C and 1050°C and a quite abruptly increase is found by making a peak at higher frequency for 1100°C and 1150°C. The peak value of  $\mu^m$  at which falling of  $\mu^r$  is observed at higher frequency which is known as ferromagnetic resonance. The linear increase of  $\mu$ ' as well as  $\mu$ <sup>"</sup> with sintering temperature is the evidence of linear relation between *μ'* and *μ'*' which can be used to

make ferrites according to the requirement of the applications. The fairly constant values of *μ'* at wide low frequency and making resonance at very higher frequency demonstrate the compositional stability which is applicable in broadband pulse transformer as well as wideband read-write heads for video recording.29



The inverse relationship between  $\mu'$  and  $H_{_c}$  is indicated in Fig. 6. It is found that *μ'* increase while Hc decline with sintering temperature which can be elucidated by Brown's relation<sup>30</sup>:

$$
H_c=\frac{2k_1}{\mu^{'}M_s}
$$

where  $k_{_I}$  is anisotropy constant,  $M_{_S}$  saturation magnetization and *μ'* is permeability. The enhancement of grain size is mainly due to motion of domain wall. This movement of domain walls tends to lower coercive force which leads to higher permeability. Low coercive force and high magnetic permeability are the main features of soft ferrite. For these properties, it can be easily magnetized and demagnetized which is widely used for electronic materials.

A VSM analysis has been employed to further study of magnetic properties of CuFe<sub>2</sub>O<sub>,</sub> which is plotted in Figure 7. It is detected that the value of magnetization is ascending sharply attaining a maximum value at a lower applied field (˂5 Oe) after that it becomes saturated upto 20 kOe for all sintering temperatures. The interception of magnetization (at  $1/H \rightarrow 0$ ) leads to value of the saturation magnetization (*M<sub>s</sub>*). It is marked that the maximum value of saturation magnetization, 63.38 emu/g obtained at *T<sub>s</sub>*=1150°C, followed by 58.09, 50.96 and 35.18 emu/g at T $_{\rm s}$ =1100°C, 1050°C and 950°C respectively. The investigated results of magnetization vs. sintering temperatures of the present study are analogous to the reported value of the CuFe $\mathrm{_2O}_4$  Ponhan $^{\text{19}}$  and Yadav. $^{\text{31}}$  The change of value of  $M_{_{\mathrm{s}}}$  with  $\mathcal{T}_{_{\mathrm{s}}}$  can be ascribed due to (i) the grain size and (ii) the contribution of  $Fe<sup>3+</sup>$  ion distribution

in A- and B-site.<sup>32, 33</sup> In previous section, larger grain size observed for greater number of domain walls due to higher sintering temperature. Increase of thermal treatment causes movement of domain walls which leads to greater magnetization. The change in the degree of inversion in CuFe $_2\rm O 4$  mainly occurs due to the exchange of Fe<sup>+3</sup> and Cu<sup>+2</sup> cations from A and B site and vice versa. This change in the degree of inversion is one of the causes of the variation of saturation magnetization with heat treatment. The number of Fe<sup>+3</sup> ions at A sites reduces as the extra Fe+3 ions in the A sites starts distributing into the B sites due to increasing the sintering temperature. Hence the number of Fe<sup>+3</sup> ions at B sites increase which is responsible for the increase in the net magnetization.

Initial permeability (*μ<sup>i</sup>* ), saturation magnetization (*Ms* ) and grain size (D) are related according Globus relationship<sup>34</sup>:

$$
\mu_i \propto \frac{M_s^2 D}{\sqrt{K_1}}
$$

where  $k<sub>i</sub>$  is the magneto-crystalline anisotropy constant. From Figure 8, it is noticed that Ms and D increases with increasing  $\mu_{_l}$  which agrees with above relation. Thus domain wall motion enhances the grain size which leads an increase of initial permeability as well as magnetization with applied field.



**Fig. 7: Dependence of permeability and coercivity on sintering temperature**



**Fig. 8: Change of saturation magnetization and grain size with permeability**

#### **Transport Properties**

The frequency dependence dielectric constant *ε'*  has been illustrated in Figure 9 for different sintering temperature. The highest value of *ε'* is observed at lower frequency by following a rapidly drop and become almost frequency independent at higher frequency which is a usual behavior of the ferrite materials. Frequency dependence dielectric constant behavior has been explained by Maxwell-Wagner<sup>35</sup> and Koop's phenomenological theory.<sup>36</sup> According



**Fig. 9: Frequency dependence dielectric constant at different temperatures**

The dependence of resistivity and dielectric constant on sintering temperature is illustrated in Figure 10 which shows an inverse relationship between them. It is noticed that the resistivity extends the values from 2x10<sup>3</sup> to 5.2x10<sup>3</sup> ohm-cm whereas dielectric constant declines from  $6.1 \mathrm{x} 10^7$  to  $5.2 \mathrm{x} 10^7$ with sintering temperature from 950°C to 1150°C. This inverse relation of dielectric constant with resistivity also can be explained According to Koops. The greater formation of  $Fe<sup>2+</sup>$  ion is due to higher sintering temperature which gives rise to electron hopping between  $Fe<sup>2+</sup>$  and  $Fe<sup>3+</sup>$  ion by reducing electrical conductivity.<sup>39, 40</sup> The movement of flow of space charge carriers restricted due to the increase of resistivity with sintering temperature. This impedes the build-up of polarization which leads to decrease of *ε'*. The finding results of resistivity and dielectric constant with sintering temperature is also evidence of above relation. The resistivity shows semiconducting nature which is applicable for high frequency devices as well as lower dielectric constant is the requirement of microwave application.

to this theory, the electron exchange between Fe<sup>2+</sup> and Fe3+ ions causes local displacement of electron which induces the polarization in ferrites.<sup>37</sup> With increase of frequency, this polarization decrease leading to reduction of dielectric constant. Similar behavior of dielectric constant has been observed by Javed $^{38}$  in CuFe $\mathrm{_2O}_4$  Nanoparticles. A very low value of dielectric constant is observed at very high frequency which is appropriate for high frequencies uses.



**Fig. 10: Relation between resistivity and dielectric constant with sintering temperature**

#### **Conclusion**

In this work, solid state reaction implies to synthesize CuFe $_{2}$ O $_{4}$  ferrites and sintered at 950°C, 1050°C, 1100°C and 1150°C for 2 hours. The physical, magnetic and electrical characteristics have been monitored due to the effects of sintering temperature. The structural property by XRD is evidence for a cubic structure and ferrite formation above 850 $\rm ^{\circ}C$ confirms by DTA and TGA. At higher sintering temperature 1150°C, the large value of Ms reduces the coercivity as a result of increase grain size as well as permeability which prove the Brown's relation. The values of  $\mathsf{M}_{_\mathrm{s}}$  as well as permeability and grain size prove the linear relation according to Globus's equation. The magnetic hysteresis represents the formation of weak ferromagnetic state which tends to strong ferromagnetic state with microstructural changes at varied sintering temperatures. The resistivity and dielectric constant shows inverse relation exhibiting normal behavior of ferrites. Therefore the sintering temperature plays vital roles

to tune the characteristic of CuFe ${_{2}O_{_{4}}}$  spinel ferrite which can find various technological applications.

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#### **Conflict of interest**

The authors do not have any conflict of interest

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